

 RMS Isolation Voltage
 VISO

 Thermal Resistance — Junction to Case
 RθJC

 — Junction to Ambient
 RθJA

 Maximum Lead Temperature for Soldering Purposes, 1/8" from case for 10 seconds
 TL

Designer's Data for "Worst Case" Conditions — The Designer's Data Sheet permits the design of most circuits entirely from the information presented. SOA Limit curves — representing boundaries on device characteristics — are given to facilitate "worst case" design.

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Preferred devices are Motorola recommended choices for future use and best overall value.

REV 2

°C/W

°C

0.28

62.5

260

### MTE53N50E

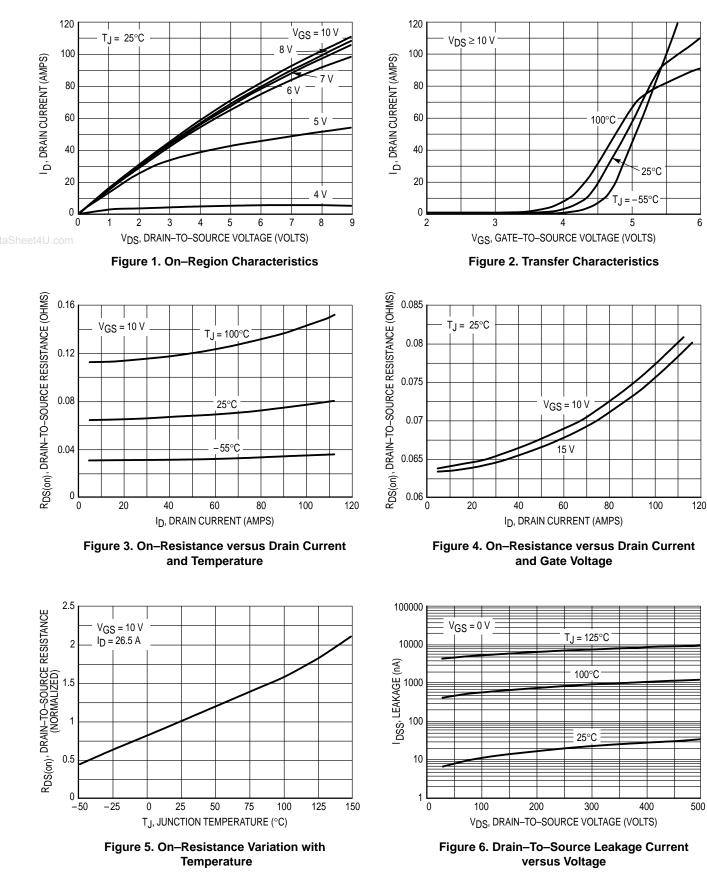
ELECTRICAL CHARACTERISTICS (T<sub>J</sub> = 25°C unless otherwise noted)

Characteristic		Symbol	Min	Тур	Max	Unit
OFF CHARACTERISTICS						
Drain–Source Breakdown Voltage (V <sub>GS</sub> = 0 Vdc, I <sub>D</sub> = 250 μAdc) Temperature Coefficient (Positive)		V(BR)DSS	500 —	560 550	_	Vdc mV/°C
Zero Gate Voltage Drain Current ( $V_{DS} = 500 Vdc, V_{GS} = 0 Vdc$ ) ( $V_{DS} = 500 Vdc, V_{GS} = 0 Vdc, T_J = 125^{\circ}C$ )		IDSS		_	10 100	μAdc
Gate–Body Leakage Current (V <sub>GS</sub> = $\pm$ 20 Vdc, V <sub>DS</sub> = 0)		IGSS	—	—	200	nAdc
ON CHARACTERISTICS (1)						
Gate Threshold Voltage ( $V_{DS} = V_{GS}$ , $I_{D} = 250 \ \mu$ Adc) Threshold Temperature Coefficient (Negative)		V <sub>GS(th)</sub>	2.0 —	3.2 —	4.0 —	Vdc mV/°C
Static Drain–Source On–Resistance ( $V_{GS}$ = 10 Vdc, I <sub>D</sub> = 26.5 Adc)		R <sub>DS(on)</sub>	—	63	80	mOhm
Drain–Source On–Voltage (V <sub>GS</sub> = Vdc) (I <sub>D</sub> = 53 Adc) (I <sub>D</sub> = 26.5 Adc, T <sub>J</sub> = 125°C)		VDS(on)		_	4.8 4.3	Vdc
Forward Transconductance ( $V_{DS}$ = 15 Vdc, $I_D$ = 26.5 Adc)		9FS	25	45	_	mhos
DYNAMIC CHARACTERISTICS						
Input Capacitance		C <sub>iss</sub>	—	14400	_	pF
Output Capacitance	(V <sub>DS</sub> = 25 Vdc, V <sub>GS</sub> = 0 Vdc, f = 1.0 MHz)	$(V_{DS} = 25 \text{ Vdc}, V_{GS} = 0 \text{ Vdc},$	_	1560	_	
Reverse Transfer Capacitance	1 – 1.0 Wi 12)	C <sub>rss</sub>	_	240	_	
SWITCHING CHARACTERISTICS (	2)					
Turn-On Delay Time	$      (V_{DD} = 250 \text{ Vdc}, \text{ I}_{D} = 53 \text{ Adc}, \\ V_{GS} = 10 \text{ Vdc}, \\ \text{R}_{G} = 4.7 \Omega ) $	<sup>t</sup> d(on)	—	67	—	ns
Rise Time		t <sub>r</sub>	_	322	—	
Turn–Off Delay Time		<sup>t</sup> d(off)	—	362	_	
Fall Time		t <sub>f</sub>	—	310	_	
Gate Charge	(V <sub>DS</sub> = 400 Vdc, I <sub>D</sub> = 53 Adc, V <sub>GS</sub> = 10 Vdc)	QT	—	474	700	nC
		Q <sub>1</sub>	—	86	_	
		Q <sub>2</sub>	—	206	_	
		Q <sub>3</sub>	—	148	_	
SOURCE-DRAIN DIODE CHARAC	TERISTICS					
Forward On–Voltage (1)	$(I_{S} = 53 \text{ Adc}, V_{GS} = 0 \text{ Vdc})$ $(I_{S} = 53 \text{ Adc}, V_{GS} = 0 \text{ Vdc}, T_{J} = 125^{\circ}\text{C})$	V <sub>SD</sub>		0.95 0.90	1.3	Vdc
Reverse Recovery Time	(I <sub>S</sub> = 53 Adc, V <sub>GS</sub> = 0 Vdc, dI <sub>S</sub> /dt = 100 A/μs)	t <sub>rr</sub>	_	720		ns
		ta	_	460	_	
		t <sub>b</sub>	_	260		
Reverse Recovery Stored Charge		Q <sub>RR</sub>	_	15		μC
NTERNAL PACKAGE INDUCTANO	) E		-	<u> </u>		-
Internal Drain Inductance (Measured from contact screw on tab to center of die) (Measured from the drain lead 0.25" from package to center of die)		LD	_	3.5 5.0		nH
Internal Source Inductance (Measured from the source lead 0.25" from package to center of die)		LS	_	5.0	_	nH

(1) Pulse Test: Pulse Width  $\leq$  300  $\mu s,$  Duty Cycle  $\leq$  2%.

(2) Switching characteristics are independent of operating junction temperature.

## **TYPICAL ELECTRICAL CHARACTERISTICS**



## POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals ( $\Delta t$ ) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ( $I_{G(AV)}$ ) can be made from a rudimentary analysis of the drive circuit so that

### $t = Q/I_G(AV)$

During the rise and fall time interval when switching a resistive load,  $V_{GS}$  remains virtually constant at a level known as the plateau voltage,  $V_{SGP}$ . Therefore, rise and fall times may be approximated by the following:

 $t_r = Q_2 \times R_G/(V_{GG} - V_{GSP})$ 

 $t_f = Q_2 \times R_G / V_{GSP}$ 

where

 $V_{GG}$  = the gate drive voltage, which varies from zero to  $V_{GG}$ 

 $R_G$  = the gate drive resistance

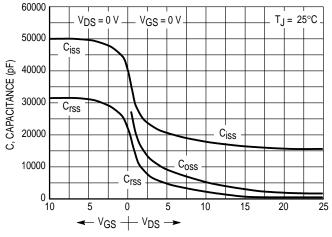
and  $Q_2$  and  $V_{GSP}$  are read from the gate charge curve.

During the turn-on and turn-off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

 $t_{d(on)} = R_G C_{iss} ln [V_{GG}/(V_{GG} - V_{GSP})]$  $t_{d(off)} = R_G C_{iss} ln (V_{GG}/V_{GSP})$  The capacitance (C<sub>ISS</sub>) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating  $t_{d(on)}$  and is read at a voltage corresponding to the on–state when calculating  $t_{d(off)}$ .

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.



GATE-TO-SOURCE OR DRAIN-TO-SOURCE VOLTAGE (VOLTS)

**Figure 7. Capacitance Variation** 

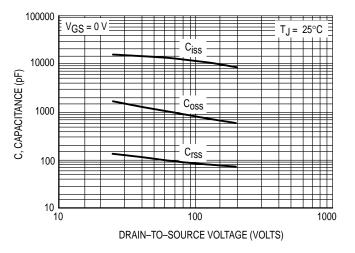


Figure 7b. High Voltage Capacitance Variation

### MTE53N50E

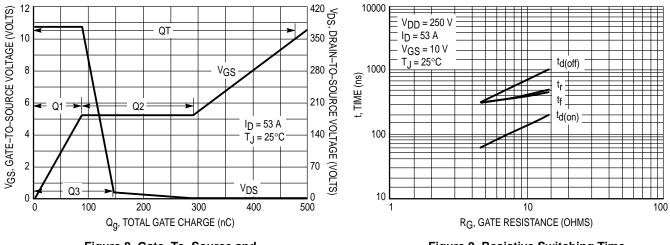
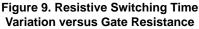


Figure 8. Gate–To–Source and <sup>Com</sup> Drain–To–Source Voltage versus Total Charge



### SAFE OPERATING AREA

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain-to-source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature (T<sub>C</sub>) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance–General Data and Its Use."

Switching between the off-state and the on-state may traverse any load line provided neither rated peak current ( $I_{DM}$ ) nor rated voltage ( $V_{DSS}$ ) is exceeded and the transition time ( $t_r$ , $t_f$ ) do not exceed 10  $\mu$ s. In addition the total power aver-

aged over a complete switching cycle must not exceed  $(T_J(MAX) - T_C)/(R_{\theta JC})$ .

A Power MOSFET designated E–FET can be safely used in switching circuits with unclamped inductive loads. For reliable operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non–linearly with an increase of peak current in avalanche and peak junction temperature.

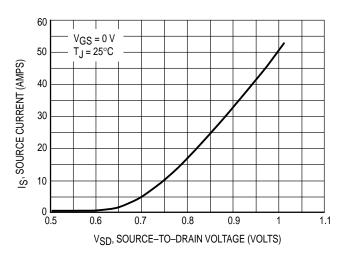
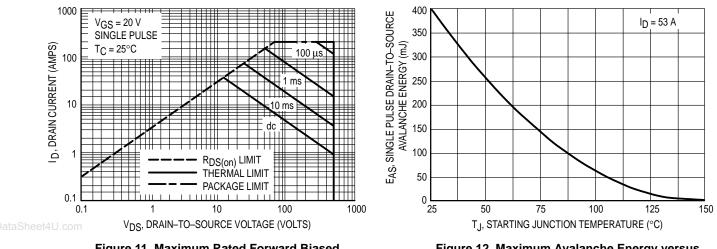


Figure 10. Diode Forward Voltage versus Current

# SAFE OPERATING AREA



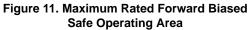


Figure 12. Maximum Avalanche Energy versus Starting Junction Temperature

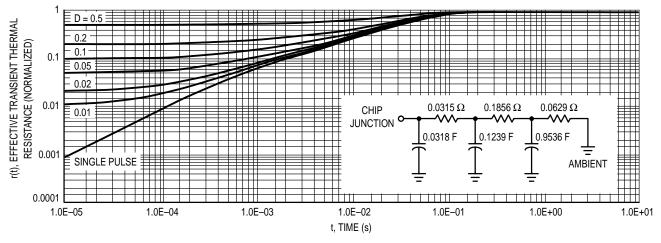


Figure 13. Thermal Response

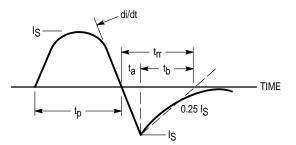
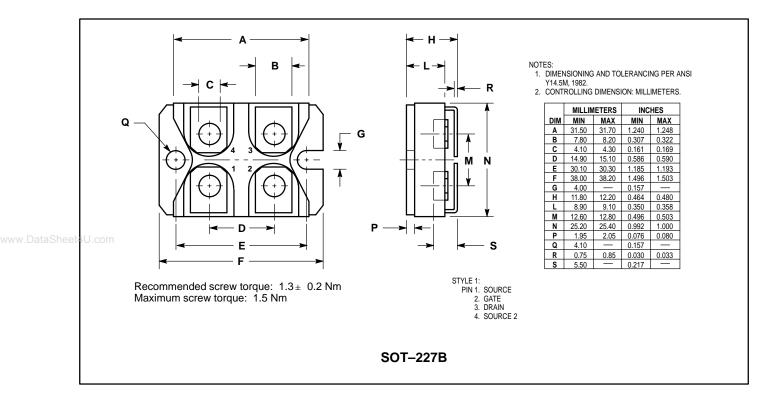


Figure 14. Diode Reverse Recovery Waveform

## PACKAGE DIMENSIONS



MTE53N50E

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