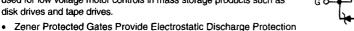
Advance Information

Medium Power Surface Mount Products

TMOS Single P-Channel with Monolithic Zener ESD Protected Gate

EZFETs™ are an advanced series of power MOSFETs which utilize Motorola's High Cell Density TMOS process and contain monolithic back-to-back zener diodes. These zener diodes provide protection against ESD and unexpected transients. These miniature surface mount MOSFETs feature ultra low RDS(on) amd true logic level performance. They are capable of withstanding high energy in the avalanche and commutation modes and the drain-to-source diode has a very low reverse recovery time. EZFET devices are designed for use in low voltage, high speed switching applications where power efficiency is important. Typical applications are dc-dc converters, and power management in portable and battery powered products such as computers, printers, cellular and cordless phones. They can also be used for low voltage motor controls in mass storage products such as disk drives and tape drives.



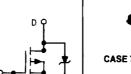
- Designed to withstand 200V Machine Model and 2000V Human Body Model
- Ultra Low RDS(on) Provides Higher Efficiency and Extends Battery Life · Logic Level Gate Drive - Can Be Driven by Logic ICs
- Miniature SO-8 Surface Mount Package Saves Board Space
- Diode Is Characterized for Use In Bridge Circuits
- · Diode Exhibits High Speed, With Soft Recovery
- IDSS Specified at Elevated Temperature
- Mounting Information for SO-8 Package Provided



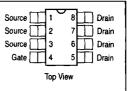


Motoroia Preferred Device

SINGLE TMOS POWER MOSFET 3.0 AMPERES 20 VOLTS $R_{DS(on)} = 0.060 \text{ OHM}$







3	6	Ш	Drain]	ı
4	5	\prod	Drain	
op V	iew			

MAXIMUM RATINGS (T_J = 25°C unless otherwise noted)

Rating	Symbol	Value	Unit
Drain-to-Source Voltage	VDSS	20	Vdc
Drain-to-Gate Voltage (R _{GS} = 1.0 MΩ)	VDGR	20	Vdc
Gate-to-Source Voltage Continuous	VGS	± 15	Vdc
Drain Current — Continuous 愛 T _A = 25°C (1) — Continuous 愛 T _A = 70°C (1) — Pulsed Drain Current (3)	а О 	6.5 3.0 52	Adc Apk
Total Power Dissipation @ TA = 25°C (1) Linear Derating Factor (1)	PD	2.5 20	Watts mW/°C
Total Power Dissipation @ T _A = 25°C (2) Linear Derating Factor (2)	PD	1.6 12	Watts mW/°C
Operating and Storage Temperature Range	T _J , T _{stg}	- 55 to 150	°C
Single Pulse Drain–to–Source Avalanche Energy — Starting $T_J = 25^{\circ}C$ ($V_{DD} = 20$ Vdc, $V_{GS} = 5.0$ Vdc, Peak $I_L = 9$ Apk, $L = 14$ mH, $R_G = 25 \Omega$)	EAS	567	mJ
Therrnal Resistance — Junction to Ambient (1) — Junction to Ambient (2)	ALeR	50 80	°C/W

Negative sign for P-Channel omitted for clarity.

When mounted on 1 inch square FR-4 or G-10 board (VGS = 10 V, @ 10 Seconds) When mounted on minimum recommended FR-4 or G-10 board (VGS = 10 V, @ Steady State)

Repetitive rating; pulse width limited by maximum junction temperature

ORDERING INFORMATION DEVICE MARKING

S3P02Z	Device	Reel Size	Tape Width	Quantity	
33F022	MMSF3P02ZR2	13″	12 mm embossed tape	2500 units	

This document contains information on a new product. Specifications and information are subject to change without notice.

Preferred devices are Motorola recommended choices for future use and best overall value

REV 1

MMSF3P02Z

ELECTRICAL CHARACTERISTICS ($T_C = 25^{\circ}C$ unless otherwise noted)

Ch	aracteristic	Symbol	Min	Тур	Max	Unit
OFF CHARACTERISTICS						
Drain-to-Source Breakdown Volta (VGS = 0 Vdc, ID = 250 μAdc) Temperature Coefficient (Positiv		V(BR)DSS	20	 23	~	Vdc mV/°C
Zero Gate Voltage Drain Current (VDS = 20 Vdc, VGS = 0 Vdc) (VDS = 20 Vdc, VGS = 0 Vdc, T	IDSS		0.05 0.2	2.0	μAdc	
Gate-Body Leakage Current (VGS	$S = \pm 15 \text{ Vdc}, V_{DS} = 0)$	IGSS		0.85	5.0	μ Ad c
ON CHARACTERISTICS(1)				·	<u></u>	
Gate Threshold Voltage (V _{DS} = V _{GS} , I _D = 250 μAdc) Threshold Temperature Coefficie	(Cpk ≥ 2.0) (1) (3) ent (Negative)	VGS(th)	1.0	1.8 3.7	3.0	Vdc mV/°C
Static Drain-to-Source On-Resist ($V_{GS} = 10 \text{ Vdc}$, $I_D = 3.0 \text{ Adc}$) ($V_{GS} = 4.5 \text{ Vdc}$, $I_D = 1.5 \text{ Adc}$)	RDS(on)	~	45 65	60 80	m£2	
Forward Transconductance (VDS	= 3.0 Vdc, I _D = 1.5 Adc) (1)	9FS	4.0	5.6	_	Mhos
DYNAMIC CHARACTERISTICS				· · · · · · · · · · · · · · · · · · ·		
Input Capacitance		C _{iss}	_	1100	2200	pF
Output Capacitance	(V _{DS} = 16 Vdc, V _{GS} = 0 Vdc, f = 1.0 MHz)	Coss		720	1440	
Transfer Capacitance	1	C _{rss}		320	640	
SWITCHING CHARACTERISTICS	2)					
Turn-On Delay Time		td(on)		90	180	ns
Rise Time	(V _{DD} = 10 Vdc, I _D = 3.0 Adc,	t _r		350	700	
Turn-Off Delay Time	$V_{GS} = 10 \text{ Vdc}, R_{G} = 6.0 \Omega$ (1)	td(off)	_	810	1620	
Fall Time		tf	-	1030	2060	
Turn-On Delay Time		td(on)	<u> </u>	230	460	ns
Rise Time	(V _{DD} = 10 Vdc, I _D = 3.0 Adc,	1 _r	-	1300	2600	
Turn~Off Delay Time	$V_{GS} = 4.5 \text{ Vdc}, R_{G} = 6.0 \Omega)$ (1)	^t d(off)		510	1020	
Fall Time		tf	-	1040	2080	1
Gate Charge		QT	_	39	55	nC
	(VDS = 16 Vdc, ID = 3.0 Adc,	Q ₁	_	2.7		
	V _{GS} = 10 Vdc) (1)	Q ₂		14.3	_	
		Q ₃	_	10.2		
SOURCE-DRAIN DIODE CHARAC	TERISTICS			·		
Forward On-Voltage(1)	$ (I_S = 3.0 \text{ Adc}, V_{GS} = 0 \text{ Vdc}) $ (1) $ (I_S = 3.0 \text{ Adc}, V_{GS} = 0 \text{ Vdc}, T_J \approx 125^{\circ}\text{C}) $	V _{SD}	<u> </u>	1,2 0.76	1.6	Vdc
Reverse Recovery Time	Time			677	<u> </u>	ns
	$(I_S = 3.0 \text{ Adc}, V_{GS} = 0 \text{ Vdc},$ $dI_S/dt = 100 \text{ A/}\mu\text{s})$ (1)	ta	_	256	_	1
	αιξίαι - 100 (ν/μα) (1)	tb	_	420		į
		 				

 ⁽¹⁾ Pulse Test: Pulse Width ≤ 300 μs, Duty Cycle ≤ 2%.
 (2) Switching characteristics are independent of operating junction temperature.
 (3) Reflects typical values.
 C_{pk} = | Max limit - Typ / 3 x SIGMA |

TYPICAL ELECTRICAL CHARACTERISTICS

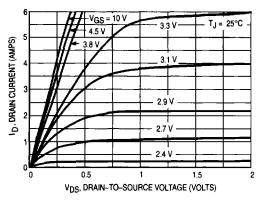


Figure 1. On-Region Characteristics

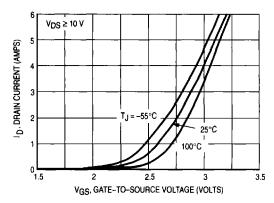


Figure 2. Transfer Characteristics

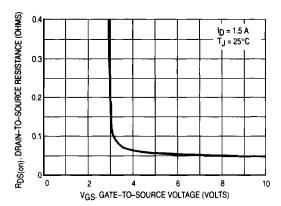


Figure 3. On-Resistance versus Gate-to-Source Voltage

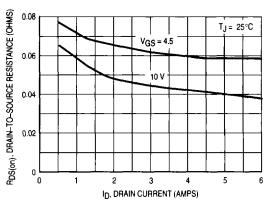


Figure 4. On–Resistance versus Drain Current and Gate Voltage

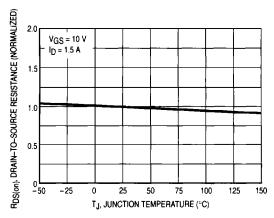


Figure 5. On–Resistance Variation with Temperature

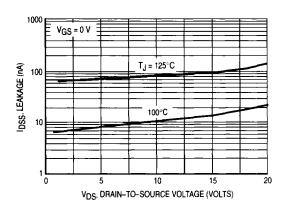


Figure 6. Drain-to-Source Leakage Current versus Voltage

Λ

POWER MOSFET SWITCHING

Switching behavior is most easily modeled and predicted by recognizing that the power MOSFET is charge controlled. The lengths of various switching intervals (Δt) are determined by how fast the FET input capacitance can be charged by current from the generator.

The published capacitance data is difficult to use for calculating rise and fall because drain–gate capacitance varies greatly with applied voltage. Accordingly, gate charge data is used. In most cases, a satisfactory estimate of average input current ($I_{G(AV)}$) can be made from a rudimentary analysis of the drive circuit so that

$$t = Q/I_{G}(AV)$$

During the rise and fall time interval when switching a resistive load, VGS remains virtually constant at a level known as the plateau voltage, VSGP. Therefore, rise and fall times may be approximated by the following:

$$t_r = Q_2 \times R_G/(V_{GG} - V_{GSP})$$

tf = Q2 x RG/VGSP

where

 V_{GG} = the gate drive voltage, which varies from zero to V_{GG} R_G = the gate drive resistance

and Q2 and VGSP are read from the gate charge curve.

During the turn-on and turn-off delay times, gate current is not constant. The simplest calculation uses appropriate values from the capacitance curves in a standard equation for voltage change in an RC network. The equations are:

$$t_{d(on)} = R_G C_{iss} ln [V_{GG}/(V_{GG} - V_{GSP})]$$

td(off) = RG Ciss In (VGG/VGSP)

The capacitance (C_{ISS}) is read from the capacitance curve at a voltage corresponding to the off–state condition when calculating $t_{d(on)}$ and is read at a voltage corresponding to the on–state when calculating $t_{d(off)}$.

At high switching speeds, parasitic circuit elements complicate the analysis. The inductance of the MOSFET source lead, inside the package and in the circuit wiring which is common to both the drain and gate current paths, produces a voltage at the source which reduces the gate drive current. The voltage is determined by Ldi/dt, but since di/dt is a function of drain current, the mathematical solution is complex. The MOSFET output capacitance also complicates the mathematics. And finally, MOSFETs have finite internal gate resistance which effectively adds to the resistance of the driving source, but the internal resistance is difficult to measure and, consequently, is not specified.

The resistive switching time variation versus gate resistance (Figure 9) shows how typical switching performance is affected by the parasitic circuit elements. If the parasitics were not present, the slope of the curves would maintain a value of unity regardless of the switching speed. The circuit used to obtain the data is constructed to minimize common inductance in the drain and gate circuit loops and is believed readily achievable with board mounted components. Most power electronic loads are inductive; the data in the figure is taken with a resistive load, which approximates an optimally snubbed inductive load. Power MOSFETs may be safely operated into an inductive load; however, snubbing reduces switching losses.

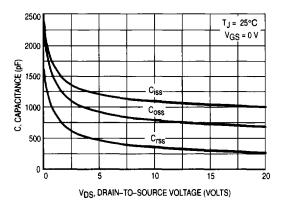
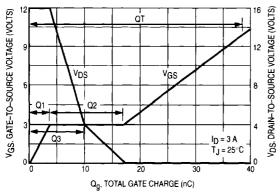


Figure 7. Capacitance Variation





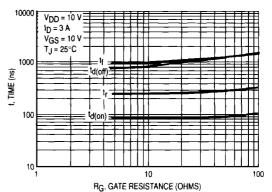


Figure 9. Resistive Switching Time Variation versus Gate Resistance

DRAIN-TO-SOURCE DIODE CHARACTERISTICS

The switching characteristics of a MOSFET body diode are very important in systems using it as a freewheeling or commutating diode. Of particular interest are the reverse recovery characteristics which play a major role in determining switching losses, radiated noise, EMI and RFI.

System switching losses are largely due to the nature of the body diode itself. The body diode is a minority carrier device, therefore it has a finite reverse recovery time, $t_{\rm rf}$, due to the storage of minority carrier charge, QRR, as shown in the typical reverse recovery wave form of Figure 11. It is this stored charge that, when cleared from the diode, passes through a potential and defines an energy loss. Obviously, repeatedly forcing the diode through reverse recovery further increases switching losses. Therefore, one would like a diode with short $t_{\rm rf}$ and low QRR specifications to minimize these losses.

The abruptness of diode reverse recovery effects the amount of radiated noise, voltage spikes, and current ringing. The mechanisms at work are finite irremovable circuit parasitic inductances and capacitances acted upon by high

di/dts. The diode's negative di/dt during t_a is directly controlled by the device clearing the stored charge. However, the positive di/dt during t_b is an uncontrollable diode characteristic and is usually the culprit that induces current ringing. Therefore, when comparing diodes, the ratio of t_b/t_a serves as a good indicator of recovery abruptness and thus gives a comparative estimate of probable noise generated. A ratio of 1 is considered ideal and values less than 0.5 are considered snappy.

Compared to Motorola standard cell density low voltage MOSFETs, high cell density MOSFET diodes are faster (shorter trr), have less stored charge and a softer reverse recovery characteristic. The softness advantage of the high cell density diode means they can be forced through reverse recovery at a higher di/dt than a standard cell MOSFET diode without increasing the current ringing or the noise generated. In addition, power dissipation incurred from switching the diode will be less due to the shorter recovery time and lower switching losses.

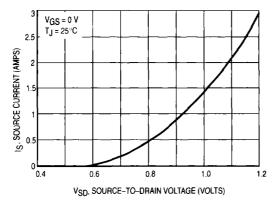


Figure 10. Diode Forward Voltage versus Current

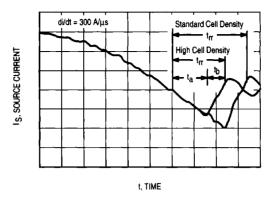


Figure 11. Reverse Recovery Time (t_{rr})

SAFE OPERATING AREA

The Forward Biased Safe Operating Area curves define the maximum simultaneous drain-to-source voltage and drain current that a transistor can handle safely when it is forward biased. Curves are based upon maximum peak junction temperature and a case temperature (T_C) of 25°C. Peak repetitive pulsed power limits are determined by using the thermal response data in conjunction with the procedures discussed in AN569, "Transient Thermal Resistance – General Data and Its Use."

Switching between the off-state and the on-state may traverse any load line provided neither rated peak current (I_{DM}) nor rated voltage (V_{DSS}) is exceeded, and that the transition time (t_r , t_f) does not exceed 10 μs . In addition the total power averaged over a complete switching cycle must not exceed ($T_{J(MAX)} - T_{C}$)/($R_{\theta JC}$).

A power MOSFET designated E-FET can be safely used in switching circuits with unclamped inductive loads. For reli-

able operation, the stored energy from circuit inductance dissipated in the transistor while in avalanche must be less than the rated limit and must be adjusted for operating conditions differing from those specified. Although industry practice is to rate in terms of energy, avalanche energy capability is not a constant. The energy rating decreases non-linearly with an increase of peak current in avalanche and peak junction temperature.

Although many E-FETs can withstand the stress of drain-to-source avalanche at currents up to rated pulsed current (IDM), the energy rating is specified at rated continuous current (ID), in accordance with industry custom. The energy rating must be derated for temperature as shown in the accompanying graph (Figure 13). Maximum energy at currents below rated continuous ID can safely be assumed to equal the values indicated.

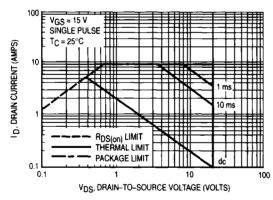


Figure 12. Maximum Rated Forward Blased Safe Operating Area

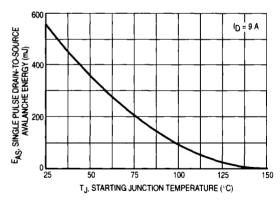


Figure 13. Maximum Avalanche Energy versus Starting Junction Temperature

TYPICAL ELECTRICAL CHARACTERISTICS

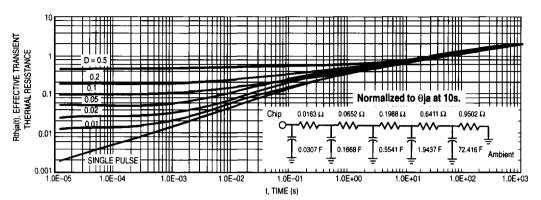


Figure 14. Thermal Response

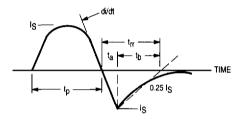


Figure 15. Diode Reverse Recovery Waveform