## Wideband/Differential Output Transimpedance Amplifier

## FEATURES

Low Cost, Wide Bandwidth, Low Noise
Bandwidth: 240 MHz
Pulse Width Modulation: 500 ps
Rise Time/ Fall Time: 1.5 ns
Input Current Noise: $3.0 \mathrm{pA} / \sqrt{\mathrm{Hz}}$ @ 100 MHz
Total Input RMS Noise: $\mathbf{2 6 . 5} \mathbf{~ n A}$ to $\mathbf{1 0 0} \mathbf{~ M H z}$
Wide Dynamic Range
Optical Sensitivity: -36 dBm @ 155.52 Mbps
Peak Input Current: $\pm 350 \mu \mathrm{~A}$

## Differential Outputs

Low Power: 5 V @ 25 mA
Wide Operating Temperature Range: $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$

## APPLICATIONS

Fiber Optic Receivers: SONET/SDH, FDDI, Fibre Channel Stable Operation with High Capacitance Detectors Low Noise Preamplifiers
Single-Ended to Differential Conversion
I-to-V Converters

## PRODUCT DESCRIPTION

The AD 8015 is a wide bandwidth, single supply transimpedance amplifier optimized for use in a fiber optic receiver circuit. It is a complete, single chip solution for converting photodiode current into a differential voltage output. The 240 M Hz bandwidth enables AD 8015 application in FDDI receivers and SON ET /SDH receivers with data rates up to 155 M bps. This high bandwidth supports data rates beyond 300 Mbps . The differential outputs drive ECL directly, or can drive a comparator/ fiber optic post amplifier.
In addition to fiber optic applications, this low cost, silicon alternative to GaAs-based transimpedance amplifiers is ideal for systems requiring a wide dynamic range preamplifier or singleended to differential conversion. The IC can be used with a standard ECL power supply ( -5.2 V ) or a PECL ( +5 V ) power supply; the common mode at the output is ECL compatible. The AD 8015 is available in die form, or in an 8-pin SOIC package.

REV. A
Information furnished by Analog Devices is believed to be accurate and reliable. However, no responsibility is assumed by Analog Devices for its use, nor for any infringements of patents or other rights of third parties which may result from its use. No license is granted by implication or otherwise under any patent or patent rights of Analog Devices.

FUNCTIONAL BLOCK DIAGRAM



Figure 1. Differential/Single-Ended Transimpedance vs. Frequency


Figure 2. Noise vs. Frequency (SO-8 Package with Added Capacitance)
© Analog Devices, Inc., 1996
One Technology Way, P.O. Box 9106, Norwood, 02062-9106, U.S.A. Tel: 617/329-4700

Fax: 617/326-8703

| Parameter | Conditions | AD8015AR |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Typ | Max |  |
| DYNAMIC PERFORMANCE <br> Bandwidth Pulse Width M odulation Rise and Fall T ime Settling Time ${ }^{1}$ | 3 dB <br> $10 \mu \mathrm{~A}$ to $200 \mu \mathrm{~A}$ Peak <br> 10\% to $90 \%$ <br> to $3 \%, 0.5 \mathrm{~V}$ Diff O utput Step | 180 | $\begin{aligned} & 240 \\ & 500 \\ & 1.5 \\ & 3 \end{aligned}$ |  | $\begin{aligned} & \mathrm{M} \mathrm{~Hz} \\ & \mathrm{ps} \\ & \text { ns } \\ & \text { ns } \end{aligned}$ |
| INPUT <br> Linear Input C urrent Range M ax Input C urrent Range Optical Sensitivity Input Stray Capacitance Input Bias Voltage | $\pm 2.5 \%$, N onlinearity Saturation <br> 155 M bps, Avg Power <br> Die, by Design <br> SOIC, by Design <br> $+V_{S}$ to $I_{\text {IN }}$ and $V_{\text {BYP }}$ | $\begin{aligned} & \pm 25 \\ & \pm 200 \\ & 1.6 \end{aligned}$ | $\begin{aligned} & \pm 30 \\ & \pm 350 \\ & -36 \\ & 0.2 \\ & 0.4 \\ & 1.8 \end{aligned}$ | 2.0 | $\mu \mathrm{A}$ <br> $\mu \mathrm{A}$ dBm pF pF |
| NOISE <br> Input Current N oise <br> Total Input RM S N oise | $\begin{aligned} & \text { D ie, Single Ended at Pout, } \\ & \text { or Differential (P Pout-N } \mathrm{Nout} \text { ), } \\ & \mathrm{C}_{\text {STRAY }}=0.3 \mathrm{pF} \\ & \mathrm{f}=100 \mathrm{M} \mathrm{~Hz} \\ & \text { DC to } 100 \mathrm{M} \mathrm{~Hz} \end{aligned}$ |  | $\begin{aligned} & 3.0 \\ & 26.5 \end{aligned}$ |  | $\mathrm{pA}_{\mathrm{nA}}^{\mathrm{n} / \sqrt{\mathrm{Hz}}}$ |
| TRANSFER CHARACTERISTICS <br> Transresistance <br> Power Supply <br> Rejection Ratio | Single Ended <br> Differential <br> Single Ended <br> D ifferential | $\begin{aligned} & 8 \\ & 16 \end{aligned}$ | $\begin{aligned} & 10 \\ & 20 \\ & 37.0 \\ & 40 \end{aligned}$ | $\begin{aligned} & 12 \\ & 24 \end{aligned}$ | $\begin{aligned} & \mathrm{k} \Omega \\ & \mathrm{k} \Omega \\ & \mathrm{~dB} \\ & \mathrm{~dB} \end{aligned}$ |
| OUTPUT <br> Differential Offset <br> Output Common-M ode Voltage Voltage Swing (Differential) <br> Output Impedance | From Positive Supply <br> Positive Input C urrent, $R_{L}=\infty$ <br> Positive Input Current, $\mathrm{R}_{\mathrm{L}}=50 \Omega$ | $\begin{aligned} & -1.5 \\ & 40 \end{aligned}$ | $\begin{aligned} & 6 \\ & -1.3 \\ & 1.0 \\ & 600 \\ & 50 \end{aligned}$ | $\begin{aligned} & 20 \\ & -1.1 \\ & \\ & 60 \end{aligned}$ | mV <br> V $\checkmark$ p-p $\mathrm{mV} p-\mathrm{p}$ <br> $\Omega$ |
| POWER SUPPLY <br> Operating Range <br> Current | $\mathrm{T}_{\text {min }}$ to $\mathrm{T}_{\text {max }}$ Single Supply Dual Supply | $\begin{aligned} & +4.5 \\ & \pm 2.25 \end{aligned}$ | $\begin{aligned} & +5 \\ & 25 \end{aligned}$ | $\begin{aligned} & +11 \\ & \pm 5.5 \\ & 26 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~mA} \\ & \end{aligned}$ |

## NOTES

${ }^{1}$ Settling $T$ ime is defined as the time elapsed from the application of a perfect step input to the time when the output has entered and remained within a specified error band symmetrical about the final value. This parameter includes propagation delay, slew time, overload recovery, and linear settling times.
Specifications subject to change without notice.

## ABSOLUTE MAXIMUM RATINGS ${ }^{\mathbf{1}}$

Supply Voltage ( $+\mathrm{V}_{\mathrm{S}}$ to - $\mathrm{V}_{\mathrm{S}}$ ). . . . . . . . . . . . . . . . . . . . . . . 12 V
Internal Power Dissipation ${ }^{2}$
Small Outline . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 0.9 Watts
Output Short Circuit Duration . . . . . . . . . . . . . . . . Indefinite
M aximum Input C urrent . . . . . . . . . . . . . . . . . . . . . . . . 10 mA
Storage T emperature Range .............. $-65^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$
Operating T emperature Range ( $\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ )
AD 8015ACHIP/AR . . . . . . . . . . . . . . . . . $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
M aximum Junction T emperature . . . . . . . . . . . . . . . . . $+165^{\circ} \mathrm{C}$
Lead Temperature Range (Soldering 10 sec ) ......... $+300^{\circ} \mathrm{C}$

## NOTES

${ }^{1}$ Stresses above those listed under "Absolute M aximum Ratings" may cause permanent damage to the device. This is a stress rating only and functional operation of the device at these or any other conditions abovethose indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.
${ }^{2}$ Specification is for device in free air: 8-pin SOIC package: $\theta_{\mathrm{JA}}=155^{\circ} \mathrm{C} / \mathrm{W}$.

## ORDERING GUIDE

| Model | Temperature <br> Range | Package <br> Description | Package <br> Option |
| :--- | :--- | :--- | :--- |
| AD 8015AR | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8-Pin Plastic SOIC | SO-8 |
| AD 8015ACHIPS | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | D ie Form |  |

## CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the AD 8015 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.


## PIN CONFIGURATION



METALIZATION PHOTOGRAPH
Dimensions shown in microns. $N$ ot to scale.


## FIBER OPTIC RECEIVER APPLICATIONS

In a fiber optic receiver, the photodiode can be placed from the $I_{\text {IN }}$ pin to either the positive or negative supply. The AD 8015 converts the current from the photodiode to a differential voltage in these applications. The voltage at the $\mathrm{V}_{\text {BYP }}$ pin is $\approx 1.8 \mathrm{~V}$ below the positive supply. T his node must be bypassed with a capacitor ( C 1 in Figures 3 and 4 below) to the signal ground. If large levels of power supply noise exist, then connecting C1 to $+\mathrm{V}_{\mathrm{S}}$ is recommended for improved noise immunity. For optimum performance, choose C 1 such that C $1>1 /(2 \pi \times 1000 \times$ $f_{\text {MIN }}$ ); where $f_{\text {MIN }}$ is the minimum useful frequency in Hz .

## PHOTODIODE REFERRED TO POSITIVE SUPPLY

Figure 3 shows the AD 8015 used in a circuit where the photodiode is referred to the positive supply. T he back bias voltage on the photodiode is $\approx 1.8 \mathrm{~V}$. T his method of referring the photodiode provides greater power supply noise immunity (PSRR) than referring the photodiode to the negative supply. The signal path is referred to the positive rail, and the photodiode capacitance is not modulated by high frequency noise that may exist on the negative rail.


Figure 3. Fiber Optic Receiver Application: Photodiode Referred to Positive Supply

## PHOTODIODE REFERRED TO NEGATIVE SUPPLY

Figure 4 shows the AD 8015 used in a circuit where the photodiode is referred to the negative supply. This results in a larger back bias voltage than when referring the photodiode to the positive supply. The larger back bias voltage on the photodiode decreases the photodiode's capacitance thereby increasing its bandwidth. The R2, C2 network shown in Figure 4 is added to decouple the photodiode to the positive supply. This improves PSRR.


Figure 4. Fiber Optic Receiver Application: Photodiode Referred to Negative Supply

## FIBER OPTIC SYSTEM NOISE PERFORMANCE

The AD 8015 maintains 26.5 nA referred to input (RTI) to 100 M Hz . Calculations below translate this specification into minimum power level and bit error rate specifications for SONET and FDDI systems. The dominant sources of noise are: $10 \mathrm{k} \Omega$ feedback resistor current noise, input bipolar transistor base current noise, and input voltage noise.
The AD 8015 has dielectrically isolated devices and bond pads that minimize stray capacitance at the $I_{I N}$ pin. Input voltage noise is negligible at lower frequencies, but can become the dominant noise source at high frequencies due to $I_{\text {IN }}$ pin stray capacitance. M inimizing the stray capacitance at the $I_{\text {IN }}$ pin is critical to maintaining low noise levels at high frequencies. The pins surrounding the $I_{\text {IN }}$ pin (Pins 1 and 3 ) have no internal connection and should be left unconnected in an application. This minimizes $I_{\text {IN }}$ pin package capacitance. It is best to have no ground plane or metal runs near Pins 1, 2, and 3 and to minimize capacitance at the $I_{\text {IN }}$ pin.
The AD 8015AR (8-pin SOIC) I IN ${ }_{\text {IN }}$ pin total stray capacitance is 0.4 pF without the photodiode. Photodiodes used for SONET or FDDI systems typically add 0.3 pF , resulting in roughly 0.7 pF total stray capacitance.

## SONET OC-3 SENSITIVITY ANALYSIS

OC-3 M inimum Bandwidth $=0.7 \times 155 \mathrm{M} \mathrm{Hz} \approx 110 \mathrm{M} \mathrm{Hz}$

$$
\text { Total Current } \mathrm{N} \text { oise }=(\pi / 2) \times 26.5 \mathrm{nA}
$$

$$
\text { = } 42 \text { nA (assuming single pole response) }
$$

To maintain a $\mathrm{BER}<1 \times 10^{-10}$ ( 1 error per 10 billion bits):
$M$ inimum current level needs to be $>13 \times$ Total Current $N$ oise

$$
=541 \mathrm{nA} \text { (peak) }
$$

A ssume a typical photodiode current/power conversion ratio

$$
=0.85 \mathrm{~A} / \mathrm{W}
$$

Sensitivity ( minimum power level) $=541 / 0.85 \mathrm{nW}$

$$
\begin{aligned}
& =637 \mathrm{nW} \text { ( peak) } \\
= & -32.0 \mathrm{dBm} \text { ( peak) } \\
= & -35.0 \mathrm{dBm} \text { ( average) }
\end{aligned}
$$

The SONET OC-3 specification allows for a minimum power level of -31 dBm peak, or -34 dBm average. $U$ sing the AD 8015 provides 1 dB margin.

## FDDI SENSITIVITY ANALYSIS

FDDI M inimum B andwidth $=0.7 \times 125 \mathrm{M} \mathrm{Hz} \approx 88 \mathrm{M} \mathrm{Hz}$

$$
\text { Total Current } \mathrm{N} \text { oise }=(\pi / 2) \times \frac{\sqrt{88 \mathrm{M} \mathrm{~Hz}}}{\sqrt{100 \mathrm{M} \mathrm{~Hz}}} \times 26.5 \mathrm{nA}
$$

$=39 \mathrm{nA}$ (assuming single pole response)

To maintain a $B E R<2.5 \times 10^{-10}$ (1 error per 4 billion bits): M inimum current level needs to be $>12.6 \times$ Total Current $N$ oise

$$
\text { = } 492 \text { nA (peak) }
$$

A ssume a typical photodiode current/power conversion ratio

$$
=0.85 \mathrm{~A} / \mathrm{W}
$$

Sensitivity ( minimum power level) $=492 / 0.85 \mathrm{nW}$

$$
\begin{aligned}
&=579 \mathrm{nW} \text { (peak) } \\
&=-32.4 \mathrm{~dB} \mathrm{~m} \text { ( peak) } \\
&=-35.4 \mathrm{~dB} \mathrm{~m} \text { ( average) }
\end{aligned}
$$

The FDDI specification allows for a minimum power level of -28 dBm peak, or -31 dBm average. U sing the AD 8015 provides 4.4 dB margin.

## THEORY OF OPERATION

The simplified schematic is shown in Figure 5. Q1 and Q3 make up the input stage, with Q3 running at $300 \mu \mathrm{~A}$ and Q 1 running at 2.7 mA . Q3 runs essentially as a grounded emitter. A large capacitor ( $0.01 \mu \mathrm{~F}$ ) placed from $\mathrm{V}_{\text {BYP }}$ to the positive supply shorts out the noise of R17, R21, and Q16. The first stage of the amplifier (Q3, R2, Q4, and C1) functions as an integrator, integrating current into the $I_{\text {IN }}$ pin. The integrator drives a differential stage (Q5, Q6, R5, R3, and R4) with gains of +3 and -3 . The differential stage then drives emitter followers (Q41, Q42, Q60 and Q61). The positive output of the differential stage provides the feedback by driving $\mathrm{R}_{\mathrm{FB}}$. The differential outputs are buffered using Q7 and Q8.
The bandwidth of the AD 8015 is set to within $\pm 20 \%$ of the nominal value, 240 M Hz , by factory trimming R 5 to $60 \Omega$. The following formula describes the AD 8015 bandwidth:

$$
\text { B andwidth }=1 /\left(2 \pi \times C 1 \times R_{F B} \times(R 5+2 r e) / R 4\right)
$$

where re (of Q 5 and Q 6 ) $=9 \Omega$ each, constant over temperature, and $R_{F B} / R 4=43.5$, constant over temperature.
The bandwidth equation simplifies, and the bandwidth depends only on the value of $C 1$ :

$$
\text { Bandwidth }=1 /(2 \pi \times 3393 \times \mathrm{C} 1)
$$



Figure 5. AD8015 Simplified Schematiic


Figure 6. Differential Output vs. Input Current


Figure 7. Single-Ended Output vs. Input Current


Figure 8. Bandwidth vs. Temperature


Figure 9. Gain vs. Frequency


Figure 10. Group Delay vs. Frequency


Figure 11. Differential Gain vs. Supply


Figure 12. Output Impedance vs. Frequency


Figure 13. Small Signal Pulse Response


Figure 14. Differential Gain vs. Input Capacitance

## APPLICATION

## 155 Mbps Fiber Optic Receiver

The AD 8015 and AD 807 can be used together for a complete 155 M bps Fiber Optic Receiver (T ransimpedance Amplifier, Post Amplifier with Signal Detect Output, and Clock Recovery and $D$ ata Retiming) as shown in Figure 16.
The PIN diode front end is connected to a single mode, 1300 nm laser source. The PIN diode has 3.3 V reverse bias, $0.8 \mathrm{~A} / \mathrm{W}$ responsivity, 0.7 pF capacitance, and 2.5 GHz bandwidth.
The AD 8015 outputs ( $\mathrm{P}_{\text {OUt }}$ and $\mathrm{N}_{\text {OUt }}$ ) drive a differential, constant impedance ( $50 \Omega$ ) low-pass $\pi$ filter with a 3 dB cutoff of 100 M Hz . The outputs of the low-pass filter are ac coupled to the AD 807 inputs (PIN and NIN ). T he AD 807 PLL damping factor is set at 10 using a $0.22 \mu \mathrm{~F}$ capacitor.
The entire circuit was enclosed in a shielded box. Table I summarizes results of tests performed using a $2^{23}-1$ PRN sequence, and varying the average power at the PIN diode.

The circuit acquires and maintains lock with an average input power as low as -39.25 dBm .


Figure 15. Bandwidth Distribution Matrix


Figure 16. 155 Mbps Fiber Optic Receiver Schematic

Table I. AD8015, AD 807 Fiber Optic Receiver Circuit: Output Bit Error Rate \& Output Jitter vs. Average Input Power

| Average Optical <br> Input Power (dBm) | Output Bit <br> Error Rate | Output Jitter <br> (ps rms) |
| :--- | :--- | :--- |
| -6.4 | Loses Lock |  |
| -6.45 | $1.2 \times 10^{-2}$ |  |
| -6.50 | $7.5 \times 10^{-3}$ |  |
| -6.60 | $9.4 \times 10^{-4}$ |  |
| -6.70 | $1 \times 10^{-14}$ | $<40$ |
| -7.0 to | $1 \times 10^{-14}$ | $<40$ |
| -35.50 | $3.0 \times 10^{-12}$ |  |
| -36.00 | $4.8 \times 10^{-10}$ |  |
| -36.50 | $2.8 \times 10^{-8}$ |  |
| -37.00 | $8.2 \times 10^{-7}$ |  |
| -37.50 | $1.3 \times 10^{-5}$ |  |
| -38.00 | $1.1 \times 10^{-4}$ |  |
| -38.50 | $1.0 \times 10^{-3}$ |  |
| -39.00 | $1.3 \times 10^{-3}$ |  |
| -39.1 | $1.9 \times 10^{-3}$ |  |
| -39.20 | $2.2 \times 10^{-3}$ |  |
| -39.25 | Loses Lock |  |
| -39.30 |  |  |

## AD8015

## AC COUPLED PHOTODIODE APPLICATION FOR

## IMPROVED DYNAMIC RANGE

AC coupling the photodiode current input to the AD 8015 (Figure 17) extends fiber optic receiver overload by 3 dB while sacrificing only 1 dB of sensitivity (increasing receiver dynamic range by 2 dB ). This application results in typical overload of -4 dBm ,
and typical sensitivity of -35 dBm . AC coupling the input also results in improved pulse width modulation performance.
C areful attention to minimize parasitic capacitance at the AD 8015 input (from the photodetector input), $\mathrm{R}_{\mathrm{AC}}$ and $\mathrm{C}_{\mathrm{AC}}$ are critical for sensitivity performance in this application. Note that $\mathrm{C}_{\mathrm{Ac}}$ of $0.01 \mu \mathrm{~F}$ was chosen for a low frequency cutoff equal to 2.2 kHz .

Figure 17. AC Coupled Photodiode Application for Improved Dynamic Range

## OUTLINE DIMENSIONS

Dimensions shown in inches and ( mm ).

## 8-Lead Small Outline IC Package (SO-8)



This datasheet has been download from:
www.datasheetcatalog.com
Datasheets for electronics components.

