

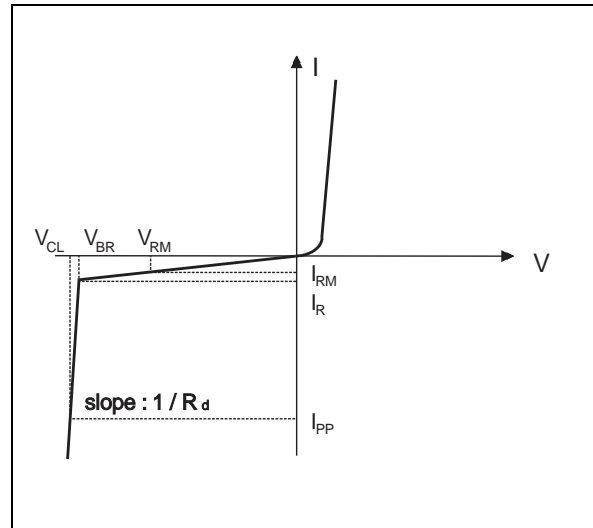
EMIF01-10018W5

ABSOLUTE MAXIMUM RATINGS ($T_{amb} = 25\text{ }^{\circ}\text{C}$)

Symbol	Parameter and test conditions	Value	Unit
V_{PP}	ESD discharge IEC1000-4-2, air discharge ESD discharge IEC1000-4-2, contact discharge ESD discharge MIL STD 883 Method 3015-6	16 9 25	kV
T_j	Junction temperature	150	$^{\circ}\text{C}$
T_{op}	Operating temperature range	-40 to + 85	$^{\circ}\text{C}$
T_{stg}	Storage temperature range	-55 to +150	$^{\circ}\text{C}$
T_L	Lead solder temperature (10 seconds duration)	260	$^{\circ}\text{C}$

ELECTRICAL CHARACTERISTICS ($T_{amb} = 25\text{ }^{\circ}\text{C}$)

Symbol	Parameter
V_{BR}	Breakdown voltage
I_{RM}	Leakage current @ V_{RM}
V_{RM}	Stand-off voltage
V_{CL}	Clamping voltage
R_d	Dynamic resistance
I_{PP}	Peak pulse current
$R_{I/O}$	Series resistance between Input and Output
C_{IN}	Input capacitance per line



Symbol	Test conditions	Min.	Typ.	Max.	Unit
V_{BR}	$I_R = 1\text{ mA}$	6	7	8	V
I_{RM}	$V_{RM} = 3\text{ V}$			100	nA
$R_{I/O}$		80	100	120	Ω
R_d	$I_{pp} = 10\text{ A}$, $t_p = 2.5\text{ }\mu\text{s}$ (see note 1)		1		Ω
C_{IN}	at 0V bias		180		pF

Note 1 : to calculate the ESD residual voltage, please refer to the paragraph "ESD PROTECTION" on pages 4 & 5

TECHNICAL INFORMATION

FREQUENCY BEHAVIOR

The EMIF01-10018W5 is firstly designed as an EMI/RFI filter. This low-pass filter is characterized by the following parameters:

- Cut-off frequency
- Insertion loss
- High frequency rejection

Fig A1: EMIF01-10018W5 frequency response curve.

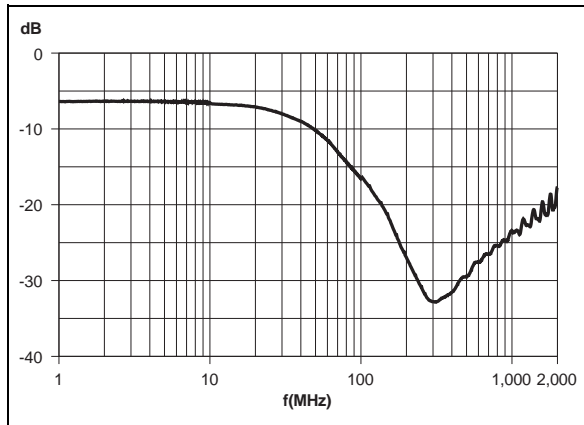
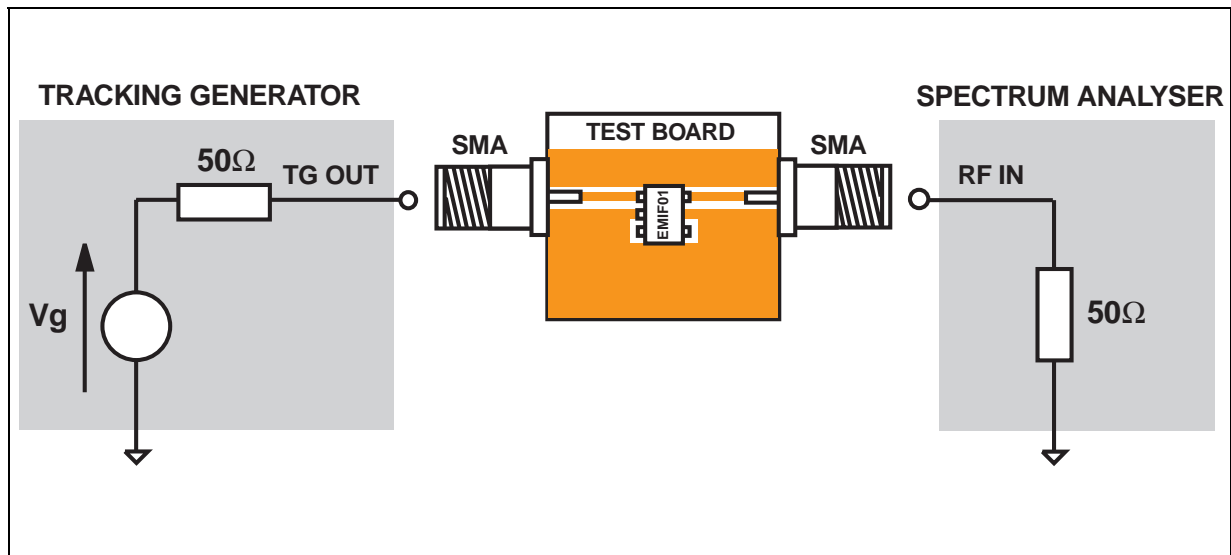


Figure A1 gives these parameters, in particular the signal rejection at the GSM frequency is about
 -24dB @ 900MHz
 -20dB @ 1800MHz

Fig. A2: Measurement conditions



EMIF01-10018W5

ESD PROTECTION

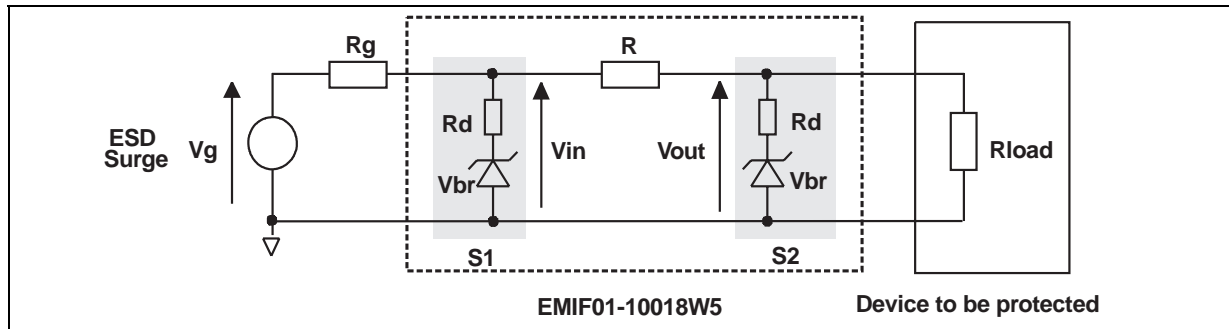
In addition to its filtering function, the EMIF01-10018W5 is particularly optimized to perform ESD protection.

ESD protection is based on the use of device which clamps at :

$$V_{CL} = V_{BR} + R_d.I_{PP}$$

This protection function is splitted in 2 stages. As shown in figure A3, the ESD strikes are clamped by the first stage S1 and then its remaining overvoltage is applied to the second stage through the resistor R. Such a configuration makes the output voltage very low at the Vout level.

Fig. A3: ESD clamping behavior.



To have a good approximation of the remaining voltages at both Vin and Vout stages, we provide the typical dynamical resistance value Rd. By taking into account these following hypothesis : $R \gg R_d$, $R_G \gg R_d$ and $R_{load} \gg R_d$, it gives these formulas:

$$V_{in} = \frac{R_g \cdot V_{br} + R_d \cdot V_g}{R_g}$$

$$V_{out} = \frac{R \cdot V_{br} + R_d \cdot V_{in}}{R}$$

The results of the calculation done for an IEC 1000-4-2 Level 4 Contact Discharge surge ($V_g=8kV$, $R_g=330\Omega$) and $V_{BR}=7V$ (typ.) give:

$$V_{in} = 31.2 \text{ V}$$

$$\mathbf{V_{out} = 7.3 \text{ V}}$$

This confirms the very low remaining voltage across the device to be protected. It is also important to note that in this approximation the parasitic inductance effect was not taken into account. This could be few tenths of volts during few ns at the Vin side. This parasitic effect is not present at the Vout side due the low current involved after the resistance R.

LATCH-UP PHENOMENA

The early ageing and destruction of IC's is often due to latch-up phenomena which mainly induced by dV/dt . Thanks to its RC structure, the EMIF01-10018W5 provides a high immunity to latch-up by integration of fast edges. (Please see the response of EMIF01-10018W5 to a 3 ns edge on Fig. A9)

The measurements done here after show very clearly (Fig. A5a & A5b) the high efficiency of the ESD protection :

- almost no influence of the parasitic inductances on Vout stage
- Vout clamping voltage very close to Vbr

Fig. A4: Measurement conditions

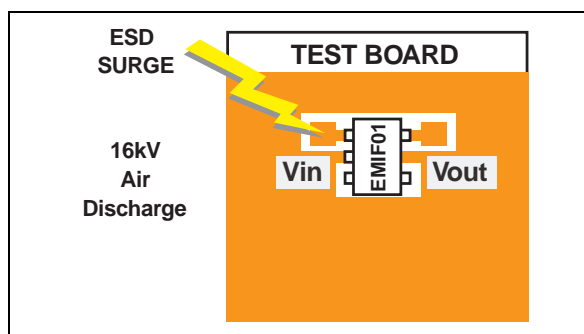
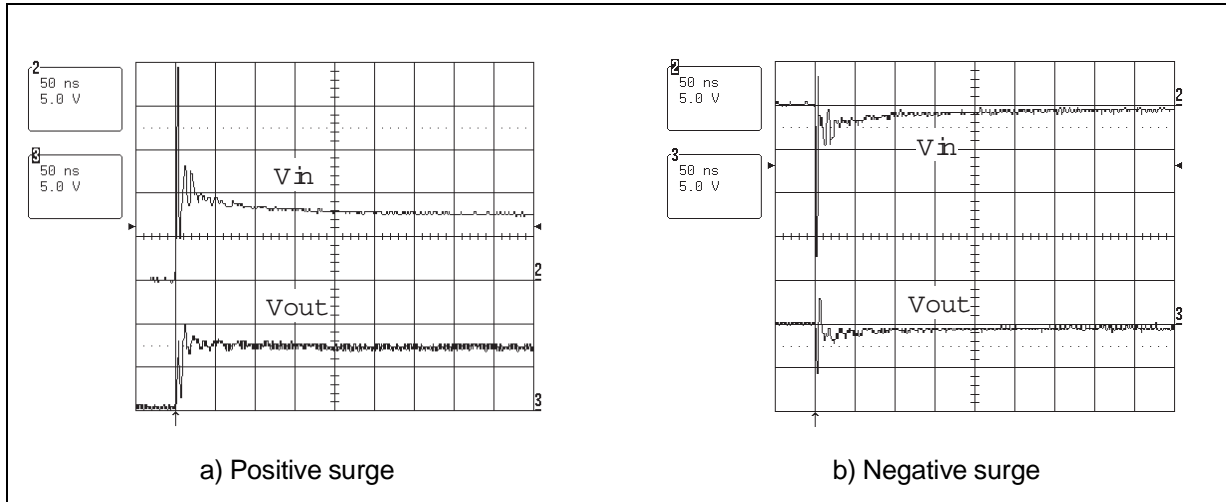
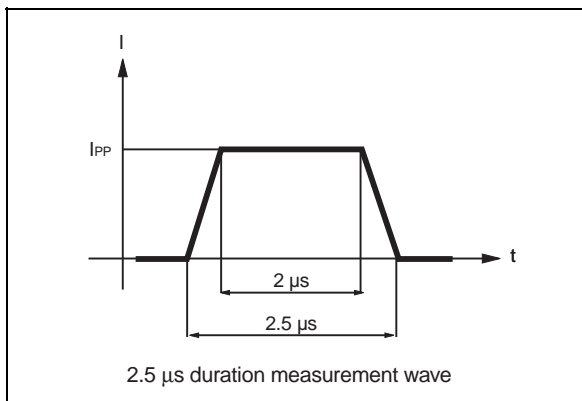


Fig. A5: Remaining voltage at both stages S1 (V_{in}) and S2 (V_{out}) during ESD surge

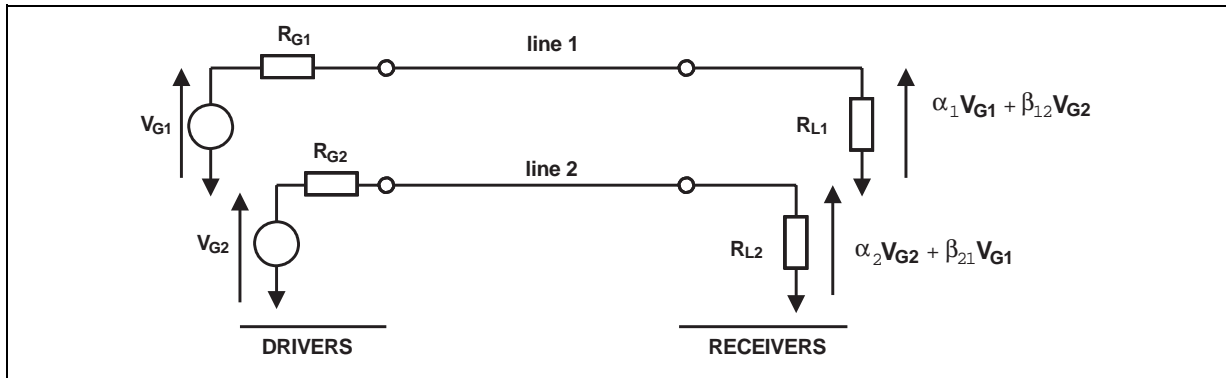
Please note that the EMIF01-10018W5 is not only acting for positive ESD surges but also for negative ones. For negatives surges, it clamps close to ground voltage as shown in Fig. A5b.

NOTE: DYNAMIC RESISTANCE MEASUREMENT**Fig. A6:** R_d measurement current wave

As the value of the dynamic resistance remains stable for a surge duration lower than 20μ s, the 2.5μ s rectangular surge is well adapted. In addition both rise and fall times are optimized to avoid any parasitic phenomenon during the measurement of R_d .

CROSTALK BEHAVIOR
1- Crosstalk phenomena

Fig. A7: Crosstalk phenomena



The crosstalk phenomena are due to the coupling between 2 lines. The coupling factor (β_{12} or β_{21}) increases when the gap across lines decreases, particularly in silicon dice. In the example above the expected signal on load R_{L2} is $\alpha_2 V_{G2}$, in fact the real voltage at this point has got an extra value $\beta_{21} V_{G1}$. This part of the V_{G1} signal represents the effect of the crosstalk phenomenon of the line 1 on the line 2. This phenomenon has to be taken into account when the drivers impose fast digital data or high frequency analog signals in the disturbing line. The perturbed line will be more affected if it works with low voltage signal or high load impedance (few k Ω). The following chapters give the value of both digital and analog crosstalk.

2- Digital Crosstalk

Fig. A8: Digital crosstalk measurement

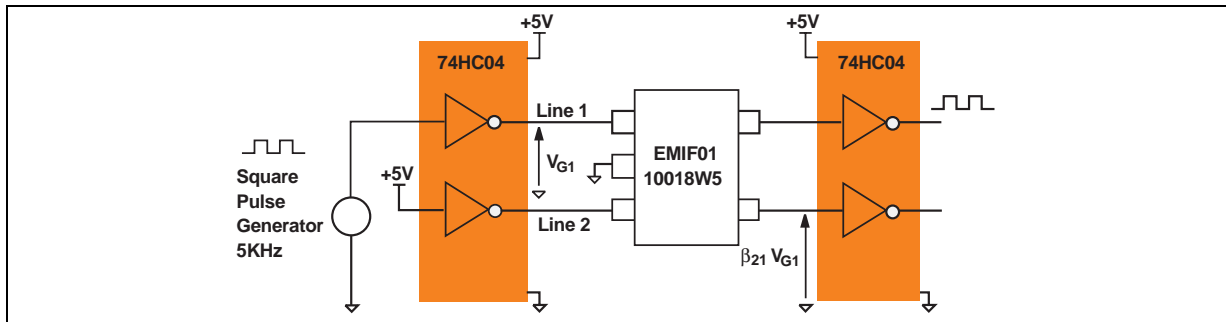
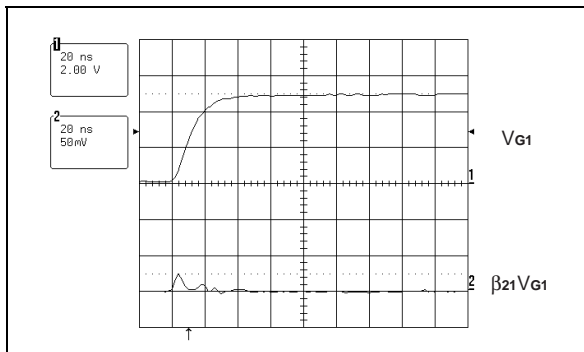


Figure A8 shows the measurement circuit used to quantify the crosstalk effect in a classical digital application.

Figure A9 shows that in such a condition signal from 0 to 5V and rise time of few ns, the impact on the disturbed line is less than 50mV peak to peak. No data disturbance was noted on the concerned line. The measurements performed with falling edges gives an impact within the same range.

Fig. A9: Digital crosstalk results



3- Analog Crosstalk

Fig. A10: Analog crosstalk measurement

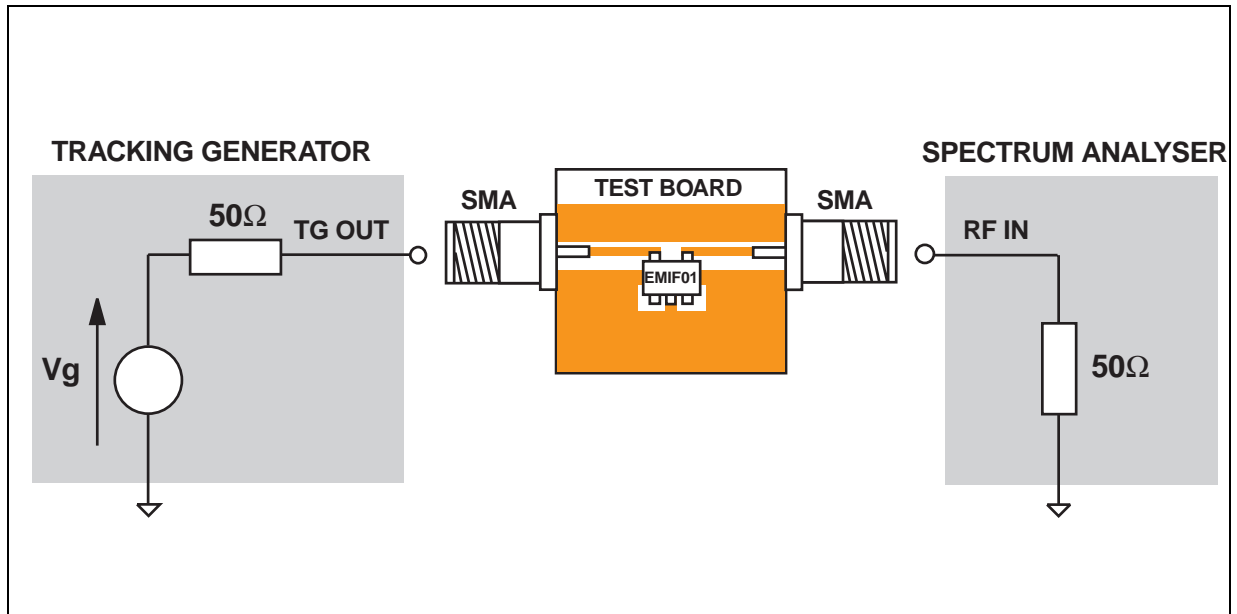


Fig. A11: Typical analog crosstalk result

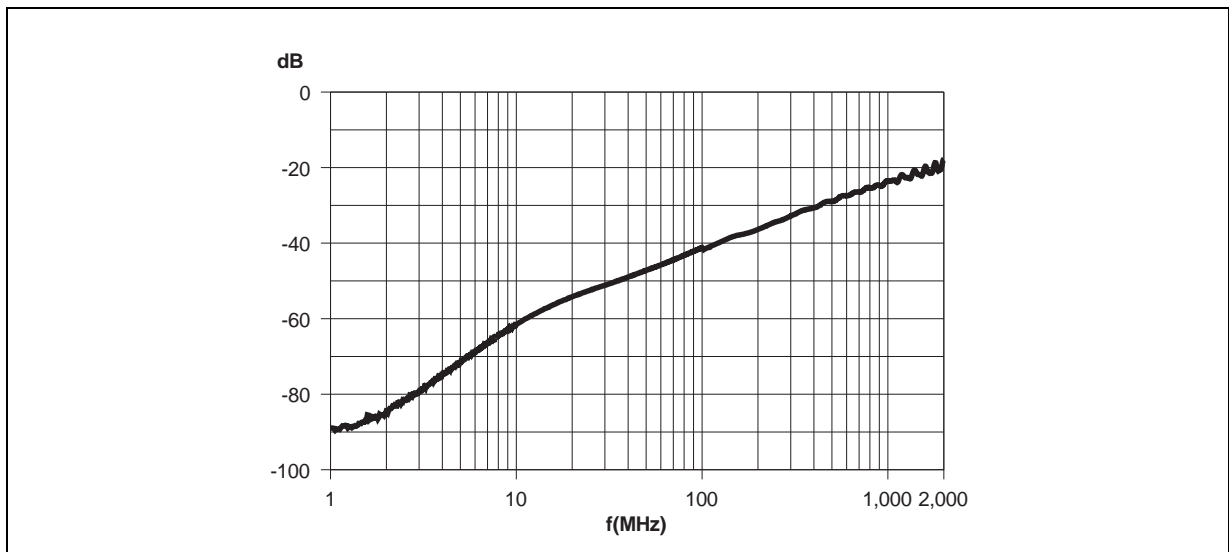
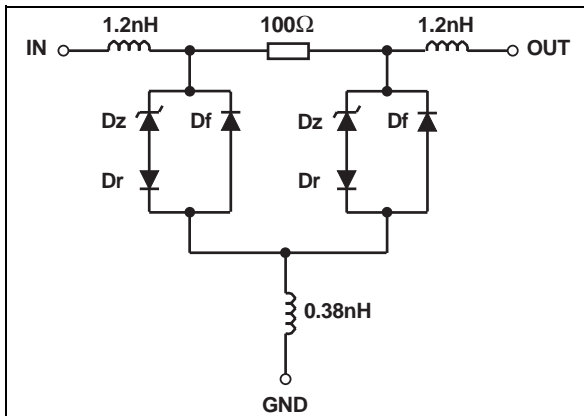


Figure A10 gives the measurement circuit for the analog application. In figure A11, the curve shows the effect of cell I/O1 on cell I/O2. In usual frequency range of analog signals (up to 100MHz) the effect on disturbed line is less than -42 dB.

EMIF01-10018W5

4 - PSpice model

Fig. A12: PSpice model of one EMIF01 cell



Note: This model is available for an ambient temperature of 27°C

Fig. A13: PSpice parameters

	Dz	Df	Dr
BV	7	1000	1000
Cjo	85p	85p	1p
IBV	1u	1u	1u
IKF	1000	1000	1000
IS	10E-15	1.016E-15	10E-15
ISR	100p	100p	100p
N	1	1.0755	0.6
M	0.3333	0.3333	0.3333
RS	1	1	1m
VJ	0.6	0.6	0.6
TT	50n	50n	1n

Fig. A14: PSpice simulation : IEC 1000-4-2 Contact Discharge response

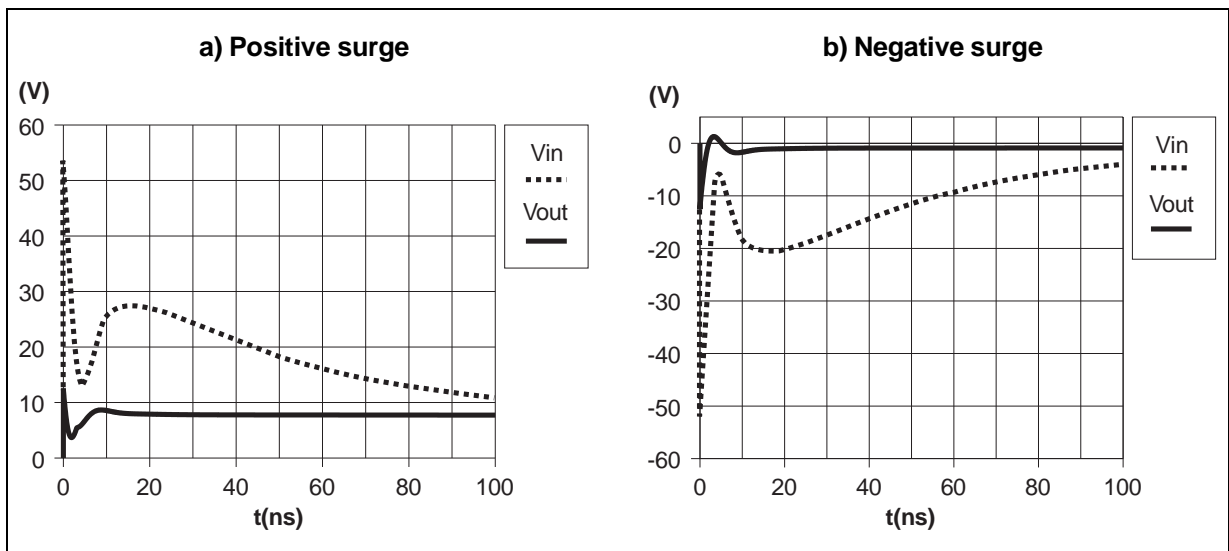
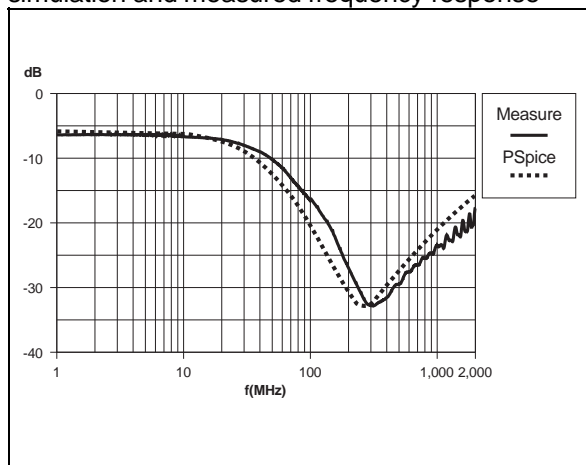
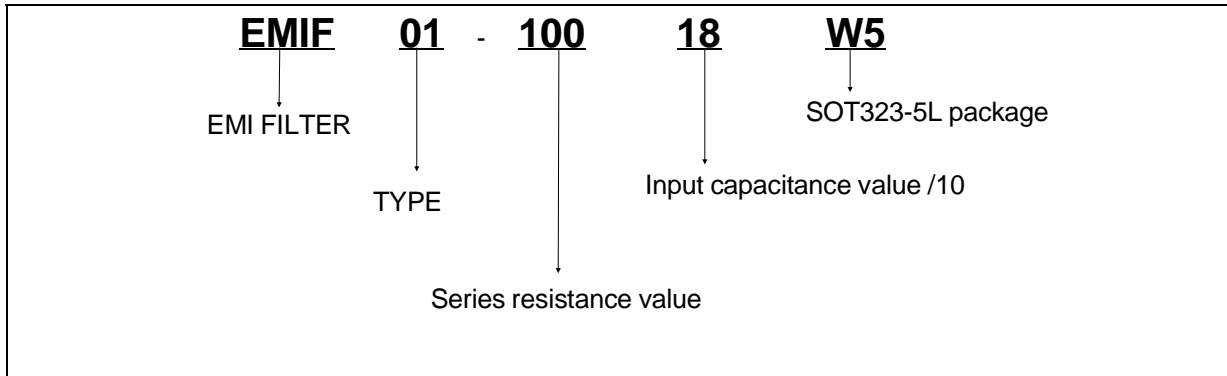


Fig. A15: Comparison between PSpice simulation and measured frequency response



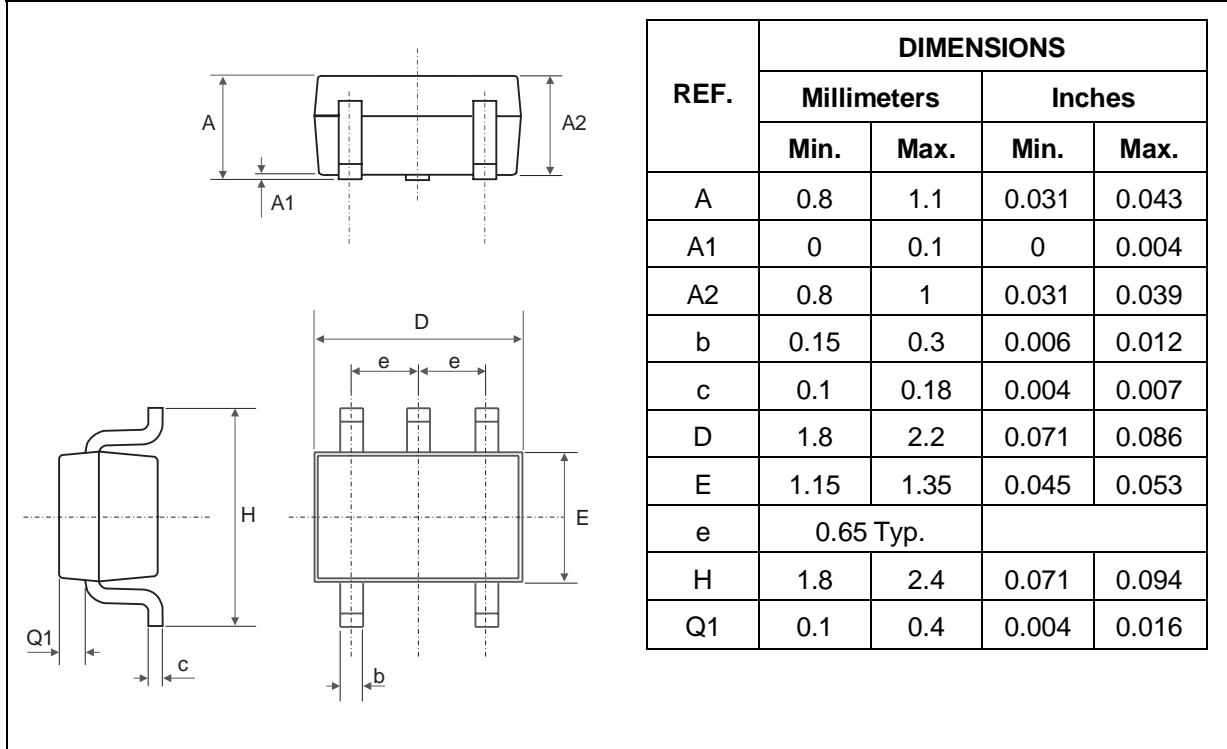
ORDER CODE



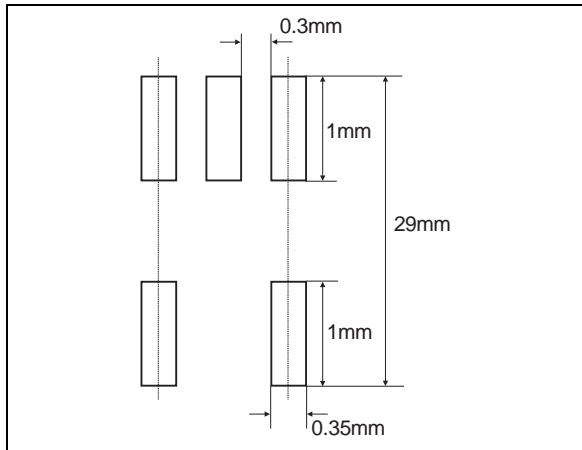
Order code	Marking	Package	Weight	Base qty	Delivery mode
EMIF01-10018W5	N12	SOT323-5L	5.4 mg	3000	Tape & reel

EMIF01-10018W5

PACKAGE MECHANICAL DATA SOT323-5L



RECOMMENDED FOOTPRINT



Mechanical specifications	
Lead plating	Tin-lead
Lead plating thickness	5µm min. 25 µm max.
Lead material	Sn / Pb (70% to 90% Sn)
Lead coplanarity	100µm max.
Body material	Molded epoxy
Flammability	UL94V-0

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